

⑩日本国特許厅(JP)

① 特許出願公開

@ 公 開 特 許 公 報 (A)

昭63 - 25933

@Int_Cl.

識別記号

广内整理番号

匈公開 昭和63年(1988)2月3日

H 01 L 21/322

M-7738-5F E-7738-5F

審査請求 未請求 発明の数 1 (全5頁)

会発明の名称

の出 頭

シリコン基板の歪付け方法

顧 昭61-169133 创特

昭61(1986)7月17日 魯田

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発明の名称 シリコン基板の歪付け方法

特許請求の範囲

- 1. シリコン基版のラップ研磨仕上した面に、エ キシマレーザー光を照射することによって。表 面に急治アモルファスシリコン層を形成したこ とを特員とするシリコン基板の歪付け方法。
- 2. エキシマレーザー光を照射することによっ て、シリコン基板のラップ研磨仕上した裏面を 瞬間的に溶散する際に、酸素雰囲気あるいは酸 **需を含む雰囲気中で溶融させ、シリコン中に腹** 素を固済したことを特徴とするシリコン基板の 至付付方法。

発明の詳細な説明

(産業上の利用分野)

本免明は半導体基板の裏面歪付け方法に関し、 特に半導体器板裏面に歪場を導入することによっ て、遊板内部の重金属等の不減物を芸板裏面に集 中して循環しようとする技術に関する。 (従来の技術)

従来、この柱の半導体基板の歪付けは、基板製 追過程において、裏面のアルミナまたはシリカ等 の確弦を打ちつけ、基板裏面を機械的に損傷させ ることによって盃を導入する方法と、半導体回路 素子製造過程において、基板裏面にリン等を過剰 に拡散あるいはイオン打込みし、結晶格子をひず ませる方法が多く用いられている。この他に、 Nd:YAGレーザーを用いた歪付け方法もあるが、実 用化には至っていない。(早襄ら(Y.Kayı[uji el al.)、ジャーナル・オブ・エレクトロケミカル・ ソ サ エ テ ィ (J. Electrochem, Soc.)。 128, 1975 (1981)).

また、茲復其面に歪付けを施す他に、茲復中に 固治している酸素を利用する方法(イントリンシ ックゲッタリング法)もある。このどき、必要と される酸器を所望の濃度で一切に固溶させるため に、引き上げ速度や回転速度を精密に制御する方 注が用いられている。

(発明が解決しようとする問題点)

基板裏面に至を与える方法のうち、細粒を用いる方法はそれが汚染線となり、デバイスの良品率を低下させることがある。不純物を拡散させる方法は高温無処理工程を必要とする。また、イオン打込みを用いる方法は、大きなイオン電流が得られないので量産性に欠ける。

Rd: YAGレーザを用いる歪付け方法では、必要なエネルギー密度を得るためにレーザービーム全面 光するので、ピーム径が小さくなり、 基 田 全面 を必要とする。 また、有効なケックリング効果を実現するために、 両 ザーガルーアができて、 基板が反ってしまうことがある。

結晶格子中に固溶している酸素を利用して欠陥 を発生させ、ゲッタリングサイトとする方法では、シリコンインゴットを製造する際に、引上げ 速度や回転速度を制御して固溶酸素濃度を一定に しなければならず、コストダウンに限界がある。

僅か1秒程度でできる。

本発明の方法は、ラップ研磨仕上面にレーザー 光を照射するものである。ラップ研磨仕上面は住 面仕上面よりも反射率が小さい。ラップ研磨仕上 面をミクロに見ると、鋭い凹凸になっており、レ ーザー光は多重乱反射され、実効的に吸収係型が 増すからである。このことは、シリコン表面層を アモルファス化するのに必要な急峻な然プロファ イルの形成に有利である。

更に、デスーデッドゾーンの形成やゲッタリング サイドの形成が必要で、このこともコストアップ の一因となっている。

"(問題点を解決するための手段)

本発明の方法は、エキシマレーザー光を照射することによって、シリコン薪販表面層をアモに対する。エキシマレーザー光に対すると化するものである。エキシマレーザー光に対するシリコンの吸収係数は、約10⁴ と非常に大きい。故に、Nd:YAGレーザー光のような独外のおいな光を照射した場合と全く異なる熱のよび時間変化がシリコン表面層で起きる。そのギー密度で、局所的に歪付けを行うことができる。

本発明の方法は、線状のレーザービームを用いて生産性を高めるものである。Nd:YACレーザーのような直径10μmのスポットビームを用いる中のような直径10μmの正付けをするのに約1分半のかる。エキシマレーザーによる線状ピームを用いると、繰り返し100Hz で、幅5 cm のに近付けをするのに

(作用)

エキシマレーザー光をシリコン基板に照射した ときの温度変化を説明するために、下記の一次元 然伝導方程式(1)を解く。

$$\frac{2\Upsilon(x_1t)}{2t} = \frac{2}{2x} \left(p \frac{2\Upsilon(x_1t)}{2x} \right) = P(x_1t) \tag{1}$$

x:深さ方向の座標

T(x,t): 温 度 (座 標 x. 時 刻 tに お け る)

P(x;l): 热 発 生 項

 はALを細かく取り、それ以外では祖く取る。為 発生項は、レーザー光の侵入深さに対応する微小 領域でのみ客でない値を持つとする。

$$\frac{Ci(T_1^{n+1}-T_1^n)}{\Delta t} = P_1^n + \sum_{n=1}^{n-1} (K_1 - \mu(T_1^n - T_1^n))$$
 (2)

Tion:時刻to.セルionの温度 Al=to-to-1

ilisa:セルiとimの間の無伝導度

Ci:セルiの熱容量

PT:時刻に、セルiの無発生項

(2)式を境界条件

$$\frac{2T(x,tA)}{2x} = 0, \quad \frac{T(x,t)}{x} = const. \quad G$$

の下で解く。

その他の使用した物性定数を表しに示す。

これに対し、赤外光であるNd: YAGレーザー光を照射したときの熱分布は、吸収係政が小さいた的に、深くかつ長時間になる。従って、Nd: YAGレーザー光を用いた場合、レーザーグループができず、かつ表面層をアモルファス化する条件は非常に厳しく、制御が難しい。

また、設需雰囲気中を、エクシマレーザー光を 通過させるとオゾンが発生する。オゾンの分子情 造は二等辺三角形で結合角(項角)は 116.8°で ある、結合距離は頂角をはさむ辺は1.278Å、底辺 は2.18Å である。

エキシマレーザー光照射によって海融したシリコンは、およそ 500~1000個のシリコン原子のクラスタが激しく運動している構造をとっている。クラスタ中は結晶シリコンとほぼ同じ構造をしている。

シリコン表面の化学吸着サイトはホロウサイト のブリッジであり、ここに酸素原子1個が吸着され、そして内部拡散していくのが酸化の初期過程 である、エキシマレーザー光で発生したオゾンが

祝1 計算に用いた定数の選

比热(J/gX)	C = 0 . 9 2 - 1 . 0	
否度(s/cm²)	ρ = 2.31	
反射率	R = 0 . G	
光 強 度(MV/cm²)	A = 1 st 193 nm	
	*2.6 st 248 nm	
吸収係数 (cm ⁻¹)	a(900℃)=2.0×106	
熟竑胜係数(cm²/s)	0(900°)	
	*0.94/(1*0.0072×T)	

表版温度を 0 でとし、パルス 編12 nsecの矩形の XFFレーザー光、光強度 2.6 M V/cm² で照射したときの、表面温度の時間変化を計算した結果を第1 図に示す。最高温度は1458でに達した。しかし、レーザー光照射後の冷却速度は速く、1 μ sec では 基級表面温度は 10 でに下がり、 100 μ sec では 基級表面温度は 0 でであった。これは、シリコン基級中の然の拡散が非常に早いためで、加熱効果は瞬間的であるといえる。

酸素分子に戻る時に放出される頂点にある酸素は、このブリッジサイトに吸着されてSi-O-Si 結合をつくる。この酸素はクラスタの速動で溶験時間内にも内部に持込まれる。故に、エキシマレーザー光で形成されたメルト構造と、エキシマレーザーで形成したオゾンにさらすと高温度の酸素温度を実現できるのである。

(寒旋例)

(実施例1)

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くてよいことが、Nd:YAGレーザーよりも、エキシャレーザーのほうがはるかに制御性が良い理由である。

用いたシリコン基板は、比低抗10Ω・cmの n型 (100) 差級で、酸素濃度は2×10¹⁷個/cm² であった。片面をラップ研磨仕上し、片面を鏡面研磨仕上した。ラップ研磨仕上げした面に、上述のUFF エキシマレーザー光を照射した、照射中に、レーザービームの長さ方向と垂直に 基板を移動し、レーザー照射による溶融板を1 mm ビッチで形成した。

溶散度は、表面のアモルファス層と内部の溶体 再結晶領域とからなっている。主たる面付近に発 を取るなっている。その外では、PU I YAGレーザーでは、PU I YAGレーザーでは、PU I YAGレーザーでは、PU I YAGレーなのできないに大きな温度勾配を実現低いるようとないできないができるのである。実 限、この重を利用して、1100でで2時間の無処理を行うと、アモルファス層が多結晶化したができた。アモルファス層が多結晶化したができた。更に、この基板を 64xビットスタテイックラングムアクセスメモリー第子製造工程に投すりた。 従来は前記のような細粒を用いて重けけけの併用が行なわれていたが本発明の方法を用いれば併用した場合と同等の良品率が得られた。

(実施併2)

実施例1と同様の条件で、存出気を設果として、ないでは、して、ないでは、このとき、シリオー照射を行った。このとき、シリモの関係を第2回に示す。バッファーガスはアルンの関係を第2回に示す。バッファーガスはアルンの発生効率が高まり、KrF エキシマレーザーを用いて、オーと固溶性素が固定との関係を調べた結果を第3回

に示す、レーザーパワーが大きいほど酸素がよく

固溶するのは、オゾンの発生量が多いのと、パワーが大きいほど溶散シリコンの温度が高く、クラスタサイズが小さくなり、激しく運動して酸素をよく取込むからである。

(発明の効果)

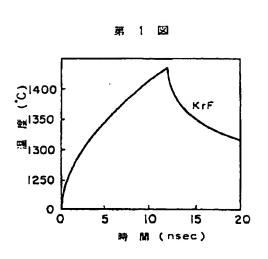
図面の簡単な説明

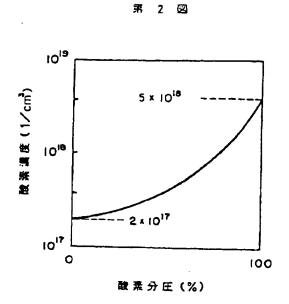
第1 図はkirF エキシマレーザー光を照射したときの表面温度の時間変化を示す図である。第2 図はkrF エキシマレーザー光を照射したときの酸素

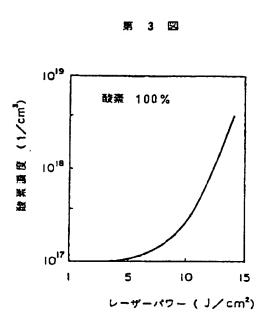
分氏と固溶酸素濃度との関係を示す図である。第 3 図はkrf エキシマレーザーのエネルギー密度と 固溶酸素濃度との関係を示す図である。

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Laid-Open Number : 63-25933

Laid-Open Date : February 3, 1988

Application Number: 61-169133

Application Date : July 17, 1986

IPC's : H 01 L 21/322

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Title : A Method for Deforming

A Silicon Substrate

Specifications

1. Title of the Invention

A Method for Deforming A Silicon Substrate

- 2. Claims
- (1) 1 A method for deforming a silicon substrate, characterized in that excimer laser beam is radiated onto a lapped and polished surface of a silicon substrate, thereby a quenching amorphous silicon layer is formed on the surface thereof.
 - (2) A method for deforming a silicon substrate,

characterized in that by use of radiation of excimer laser beam, when a lapped and polished rear side of a silicon substrate is melted instantaneously, it is melted in oxygen atmosphere or atmosphere including oxygen, thereby oxygen is solved in silicon.

3. Detailed Description of the Invention [Field of the Invention]

The present invention relates to a method for deforming the rear side of a silicon substrate, more specifically, the present invention relates to a technology for intensively capturing impurities such as heavy metals in a substrate on the rear side of a substrate by introducing a deformed portion on the rear side of a semiconductor substrate.

Conventionally, with respect to this kind of deformation of a semiconductor substrate, have been widely used a method wherein fine particles such as almina or silica or so are blasted onto a rear side, and the rear side of a substrate is damaged mechanically, thereby deformation is introduced, and another method wherein in the manufacturing process of semiconductor circuit elements, phosphorus and so forth are excessively sprayed onto or ion implemented into the rear side of a substrate, thereby crystal lattice is distorted. Besides the above methods, there is a method for deforming

buy use of Nd:YAG laser, however, this has not yet been in

[Prior Art]

practical applications. (Y.Hayafuji. et al., The Journal of Electrochemical Society (J.Electrochem.Soc.), 128, 1975 (1981)).

And besides deforming the rear side of a substrate, there is a method wherein oxygen solved in a substrate is utilized (intrinsic gettering method). In this method, in order to solve a necessary amount of oxygen evenly at a desired concentration, a method for controlling pulling up speed and rotational speed in a minute manner.

[Problems to be Solved by the Invention]

Among the above methods for giving deformation on a substrate rear side, in the method using fine particles, those fine particles become a source of pollution, decreasing the good product ratio of devices. While the method by diffusing impurities requires a heat treatment at high temperature. And in the method using ion implementation, it is not possible to obtain large ion current, as a result, it lacks of mass production property.

In the deformation method using Nd:YAG laser, a laser beam is radiated intensively in order to obtain necessary energy density, therefore the beam diameter therein is apt to be small, and long hours are required for deforming a whole substrate surface. And when a pulse beam at high energy density is radiated in order to realize an effective

gettering effect, there may be a laser group, and a substrate may become warped.

While, in the method wherein flaws are made by use of oxygen solved in crystal lattice and gettering sites are made, in manufacturing a silicon ingot, it is necessary to control pulling up speed and rotational speed to make solved oxygen concentration constant, as a result, there is a limit in cost reduction. Further, it requires formation of death - dead zone and formation of gettering sides, which also cause cost increase.

[Means to Solve the Problems]

A method according to the present invention is one wherein excimer laser beam is radiated, thereby a silicon substrate surface layer is made amorphous. The absorption coefficient of silicon to excimer laser beam is as extremely large as about 106. Accordingly, a heat distribution and time changes completely different from those in the case where a beam of small absorption coefficient such as Nd:YAG laser beam occur on a silicon surface layer. As a result, according to the present invention, it is possible to make deformation locally at far lower energy density than by Nd:YAG laser beam.

A method according to the present invention is one wherein productivity is increased by use of a linear laser beam. By use of a spot beam of diameter 40 µm like Nd:YAG

laser, it will take about one minute and a half to give deformation on a whole 4-inch substrate surface. In contrast, by use a linear beam by excimer laser, of width 5cm at 100 Hz repeatedly, it will take only one second or so to deformation on a whole 4-inch substrate surface.

A method according to the present invention is one wherein a laser beam is radiated onto a lapped and polished surface. A lapped and polished surface has a reflection ratio smaller than that of a specular surface. A lapped and polished surface has microfine and sharp concaves and convexes, by which a laser beam is irregularly reflected in multiple, thereby its absorption coefficient is increased substantially. This is very advantageous for formation of a rapid heat profile necessary for making a silicon surface layer amorphous.

Another method according to the present invention is one wherein excimer laser beam is radiated in oxygen atmosphere or atmosphere including oxygen. Oxygen is ozonized by excimer laser beam. Ozone is apt to be taken in melted silicon, and increases solved oxygen concentration at solidification. When oxygen is taken in a substrate, it becomes a gettering site where flaws are generated. Since this gettering site and deformation generated by making the above silicon surface layer amorphous exist almost in a single area, therefore, it is more effective than the case

of only deformation by making the surface amorphous.

[Action]

So as to explain temperature changes at radiation of excimer laser beam onto a silicon substrate, the following one-dimensional heat transmission equation (1) is solved.

$$\frac{2T(x_1t)}{2t} - \frac{2}{2x} \left(p \frac{2T(x_1t)}{2x} \right) = P(x_1t)$$
 (1)

wherein, x : coordinate in depth direction

 $T(x_1t)$: temperature (at coordinate x and time t)

 $P(x_1t)$: heat generation item

The above one-dimensional heat transmission equation is rewritten into a difference equation as shown in the equation (2) shown later herein, and analyzed. Now suppose that a silicon substrate is divided into microfine areas, and suppose the heat flow-in and flow-out from another microfine area adjacent to an area. Dividing into microfine areas is made in one diminution from surface to depth direction. The size of microfine areas is made fine at surface, while coarse at inside. Laser pulse time is divided into time Δt that is 10 minutes shorter than the above time, and heat amount flowing in from external side within each time Δt is given instantaneously to the first of each Δt and then become appropriate. Δt is taken short at time corresponding to laser pulse, while taken rough at other. Suppose that the heat generation item has other value than

zero only at microfine area corresponding to intrusion depth of laser beam.

$$\frac{Ci(T_i^{n+1}-\Gamma_i^n)}{\Delta t} = P_i^n \sum_{n=1}^{\infty} (T_i T_n - \Gamma_i^n). \tag{2}$$

wherein, T n 1+m : temperature at time tn and cell i+m $\Delta t = t n - t n - 1$

1 K 1+m : heat transmission degree between cells i and i+m

C1 : heat capacity of cell i

P n 1 : Heat generation item at time tn and cell i

The equation (2) is solved under the following boundary

condition.

$$\frac{2T(x,th)}{2x}\bigg|_{x=0}=0. \quad \frac{T(x,t)}{x}\bigg|_{x=\infty}=const. \tag{3}$$

Other physical constants used herein are shown in TABLE 1.

TABLE 1 Constants used in calculation

Specific heat (j/gx)	C - 0.91 - 1.0
Density (g/cm3)	ρ = 2.31
Reflection ratio	R = 0.6
Light intensity (MW/cm ²)	l = 1 at 193 nm
	= 2.6 at 248 nm
Absorption coefficient (cm-1)	a (900°C) = 2.0 x 106
Heat diffusion coefficient (cm ² /s)	D (900°C)
	$=0.94 / (1 + 0.0072 \times T)$

The results of calculation of time changes of surface temperature in the case when a rectangular KrF laser beam with pulse width 12 nsec was radiated at light intensity 2.6 MW/cm² are shown in FIG.1. The maximum temperature reached 1450°C. However, the cooling speed after laser beam radiation was low, and the substrate surface temperature went down to 10°C at 1 μ sec, and the substrate surface temperature was 0°C at 100 μ sec. This is because the heat diffusion in a silicon substrate is very fast, and it may be said that heating effect is instantaneous.

In contrast, heat distribution in the case of radiation of Nd:YAG laser beam that is an infrared light is deep and

lasts long since the absorption coefficient thereof is small. Consequently, in the case using Nd:YAG laser beam, laser groups are not formed, and conditions for making a surface layer amorphous are very severe, so control becomes difficult.

And, when excimer laser beam passes through oxygen atmosphere, ozone is generated. The molecular structure of ozone is of an isosceles triangle, and its bond angle (apex angle) is 116.8°. The bond distance at a side forming the apex angle is 1.278Å, while that at bottom side is 2.18Å.

Silicon melted by excimer laser beam radiation has a structure wherein about 500 to 1000 clusters of silicon atom are moving actively. The structure in a cluster is almost same as the structure of silicon.

The chemical absorption site on silicon surface is a bridge of a hollow site, and one oxygen atom is absorbed therein, and it diffuses inside, which is the initial process of oxidation. Oxygen at the apex where ozone generated by excimer laser beam gets back into oxygen molecular is absorbed into this bridge site to form an Si-O-Si combination. Thus oxygen is brought inside even during melting by movement of clusters. Accordingly, when it is exposed to a melted structure formed by excimer laser beam, and ozone formed by excimer laser, it is possible to realize a high oxygen concentration.

[Description of Preferred Embodiments]

[Preferred Embodiment 1]

As excimer laser, KrF excimer laser with wave length 248 nm was employed. The pulse width (FWHM) was 12 nsec, repetition was at 90 Hz. Time average light intensity was 60 M, that is, energy per one pulse was about 0.7 J. This laser pulse was converged in linear shape by a cylindrical lens. The beam size was 5 x 0.01 cm. Energy density was 14 J/cm³. This energy density is smaller by about two digits than the case using Nd:YAG laser, but the absorption coefficient thereof is larger by five digits, therefore, such a small value as this is sufficient. And energy density may be small, and these are reasons for that controllability of excimer laser is better than that of Nd:YAG laser.

The silicon substrate used herein was an n-type (100) substrate with specific resistance $10\Omega cm$, and the oxygen concentration thereof was 2 x 10^{17} pieces/cm³. One surface of the substrate was lapped and polished, while the other surface was polished into specular finish. The above KrF excimer laser beam was radiated onto the lapped and polished surface. During radiation, the substrate was moved at right angle with the length direction of the laser beam, and melted flows by laser radiation were formed at pitch 1 mm.

A melted flaw comprises an amorphous layer at the surface, and a melted recrystalized area at the inside. Main

deformation is concentrated on near the boundary between the amorphous layer and the melted recrystalized area. The size thereof is determined by temperature curve at laser radiation. Since it is possible to realize a far large temperature curve by excimer laser than by Nd: YAG laser, accordingly, it is possible to sufficiently create crystal flaws to become gettering site even with a low energy density with which laser groups are not formed. Actually, when heat treatment was carried out at 1100°C for two hours by use of this deformation, the amorphous layer became polycrystalline, and it was possible to create 105 to 107 pieces/cm3 of surface flaws. Further, the substrate was charged into manufacturing process of 64-Kbit static random access memory element. Conventionally, the method for deforming by use of such fine particles as mentioned above and the intrinsic gettering method have been employed in combination, however, according to a method under the present invention, it has been possible to obtain the same good product ratio as by the combination of conventional methods.

[Preferred Embodiment 2]

Under the same conditions as in the first preferred embodiment, atmosphere was made oxygen, and laser radiation was carried out. At this moment, the oxygen amount to be

solved into silicon depends on oxygen partial pressure. This relation is shown in FIG.2. As a buffer gas, argon was used. When ArF excimer laser is employed, ozone generation efficiency is increased, and the same amount of oxygen may be solved at oxygen partial pressure lower than in the case using KrF excimer laser.

The results of investigation on the relation between laser power and solved oxygen concentration by use of KrF excimer laser are shown in FIG.3. The larger the laser power is, the more oxygen is solved, because much of ozone is generated, and the larger the power is, the higher the temperature of solved silicon gets, the smaller the size of clusters becomes and the more actively clusters move and take in oxygen more.

[Effect of the Invention]

As described heretofore, an extrinsic gettering method according to the present invention using excimer laser has the following effects. 1) It is clean. 2) The method wherein impurities are diffused as mentioned in the section Prior Art requires heat treatment at high temperature, but the present invention may be embodied at room temperature. 3) Only a substrate surface gets at high temperature, therefore the above method may be carried out even after device process. 4) The above method does not depend on transmission types and oxygen concentration of substrate. 5) The above

method is so soft as not to cause camber. As a consequence, the ebove method according to the present invention may be said to be an effective method for giving deformation for future silicon substrates and so forth with large diameter.

4. Brief Description of the Drawings

FIG.1 is a graph showing time changes of surface temperature at radiation of KrF excimer laser beam. FIG.2 is a graph showing the relation between oxygen partial pressure and solved oxygen concentration at radiation of KrF excimer laser beam. FIG.3 is a graph showing the relation between energy density and solved oxygen concentration of KrF excimer laser.

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[FIG.1]	Temperature ($^{\circ}$) Time (nsec)
[FIG.2]	Oxygen concentr	ation
	OXygenxygen par	tial pressure
[FIG.3]	IG.3] Oxygen concentration	
	Oxvgen Las	er power